

# *Narrow-band Frequency Modulation*

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# Summary

- **Narrowband Frequency Modulation**
- **Wideband Frequency Modulation**

# Narrow-Band Frequency Modulation

- Narrow-Band FM means that the FM modulated wave has narrow bandwidth.
- Consider the single-tone wave as a message signal:

$$m(t) = A_m \cos(2\pi f_m t)$$

- FM signal
  - Instantaneous frequency

$$\begin{aligned} f_i(t) &= f_c + k_f A_m \cos(2\pi f_m t) \\ &= f_c + \Delta f \cos(2\pi f_m t) \end{aligned} \quad \Delta f = k_f A_m$$

- Phase

$$\begin{aligned} \theta_i(t) &= 2\pi \int_0^t f_i(\tau) d\tau = 2\pi \left[ f_c t + \frac{\Delta f}{2\pi f_m} \sin(2\pi f_m t) \right] \\ &= 2\pi f_c t + \frac{\Delta f}{f_m} \sin(2\pi f_m t) \end{aligned}$$


- Definitions

- Phase deviation of the FM wave  $\beta = \frac{\Delta f}{f_m}$

- Modulation index of the FM wave:  $f_m$

- Then, FM wave is

$$s(t) = A_c \cos[2\pi f_c t + \beta \sin(2\pi f_m t)]$$

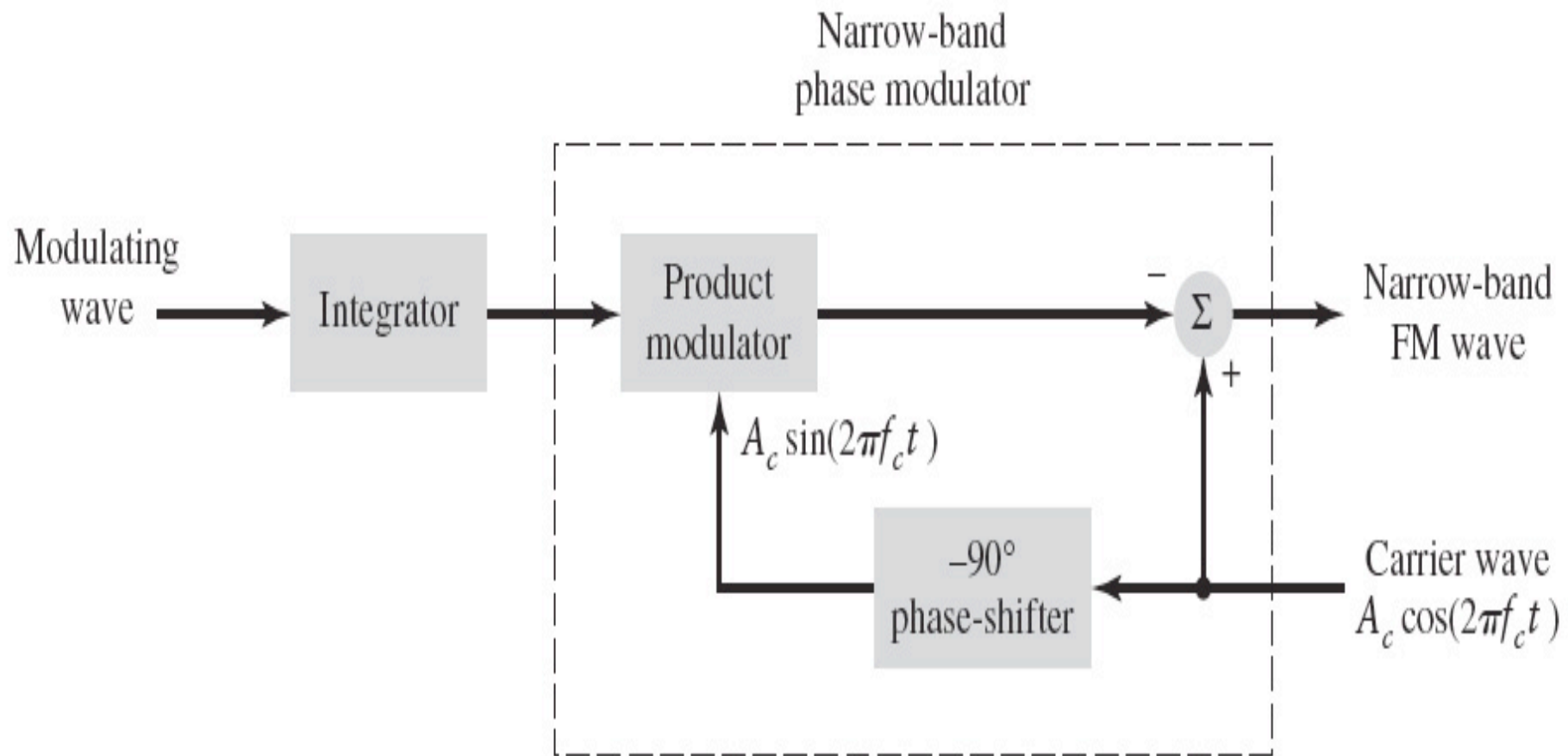

$$s(t) = A_c \cos(2\pi f_c t) \cos(\beta \sin(2\pi f_m t)) - A_c \sin(2\pi f_c t) \sin(\beta \sin(2\pi f_m t))$$

- To be narrow-band FM,  $\beta$  should be small.

- For small  $\beta$  compared to 1 radian, we can rewrite

$$\cos[\beta \sin(2\pi f_m t)] \approx 1, \quad \sin[\beta \sin(2\pi f_m t)] \approx \beta \sin(2\pi f_m t)$$


$$s(t) \approx A_c \cos(2\pi f_c t) - \beta A_c \sin(2\pi f_c t) \sin(2\pi f_m t)$$



**FIGURE 4.4** Block diagram of an indirect method for generating a narrow-band FM wave.

# Polar Representation from Cartesian

- Consider the modulated signal

$$s(t) = a(t) \cos(2\pi f_c t + \phi(t))$$

which can be rewritten as

$$s(t) = s_I(t) \cos(2\pi f_c t) - s_Q(t) \sin(2\pi f_c t)$$

where

$$s_I(t) = a(t) \cos(\phi(t)), \quad \text{and,} \quad s_Q(t) = a(t) \sin(\phi(t))$$

and

$$a(t) = [s_I^2(t) + s_Q^2(t)]^{\frac{1}{2}}, \quad \text{and} \quad \phi(t) = \tan^{-1} \left[ \frac{s_Q(t)}{s_I(t)} \right]$$

- Approximated narrow-band FM signal can be written as

$$s(t) \approx A_c \cos(2\pi f_c t) - \beta A_c \sin(2\pi f_c t) \sin(2\pi f_m t)$$

- Envelope

$$a(t) = A_c [1 + \beta^2 \sin^2(2\pi f_m t)] \approx A_c \left(1 + \frac{1}{2}\beta^2 \sin^2(2\pi f_m t)\right)$$

- Maximum value of the envelope

for small  $\beta$

$$A_{\max} = A_c \left(1 + \frac{1}{2}\beta^2\right)$$

- Minimum value of the envelope

$$A_{\min} = A_c$$

- The ratio of the maximum to minimum value

$$\frac{A_{\max}}{A_{\min}} = \left(1 + \frac{1}{2}\beta^2\right)$$

- Rewriting the approximated narrow-band FM wave is

$$s(t) \approx A_c \cos(2\pi f_c t) + \frac{1}{2}\beta \cos(2\pi(f_c + f_m)t) - \frac{1}{2}\beta A_c \cos(2\pi(f_c - f_m)t)$$

- Average power

$$P_{\text{av}} = \frac{1}{2}A_c^2 + \left(\frac{1}{2}\beta A_c\right)^2 + \left(\frac{1}{2}\beta A_c\right)^2 = \frac{1}{2}A_c^2(1 + \beta^2)$$

- Average power of the unmodulated wave

$$P_c = \frac{1}{2}A_c^2$$



- Ration of the average power to the power of the unmodulated wave

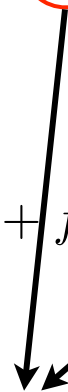
$$\frac{P_{av}}{P_c} = 1 + \beta^2$$

- Comparison with the AM signal
  - Approximated Narrow-band FM signal

$$s(t) \approx A_c \cos(2\pi f_c t) + \frac{1}{2}\beta \cos(2\pi(f_c + f_m)t) - \frac{1}{2}\beta A_c \cos(2\pi(f_c - f_m)t)$$

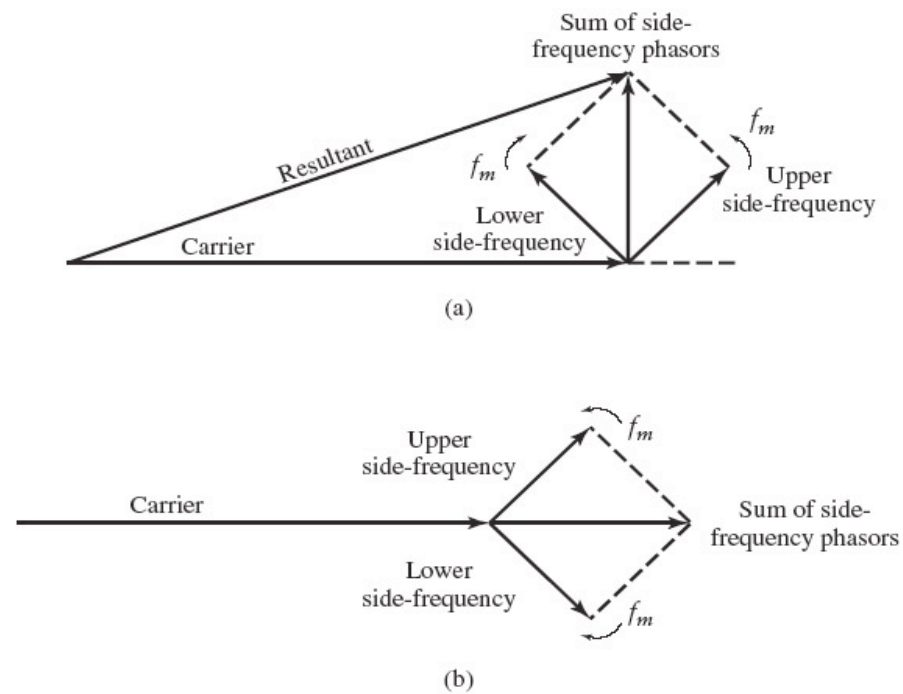
- AM signal

$$s_{AM}(t) = A_c \cos(2\pi f_c t) + \frac{1}{2}\mu A_c \{ \cos[2\pi(f_c + f_m)t] + \cos[2\pi(f_c - f_m)t] \}$$



difference between the narrow-band FM and AM waves

- Bandwidth of the narrow-band FM:  $2f_m$
- Phasor interpretation



**FIGURE 4.5** Phasor comparison of narrow-band FM and AM waves for sinusoidal modulation. (a) Narrow-band FM wave. (b) AM wave.

[Ref: Haykin & Moher, Textbook]

- Angle

$$\theta(t) = 2\pi f_c t + \phi(t) = 2\pi f_c t + \tan^{-1}(\beta \sin(2\pi f_m t))$$

- Using the power series of the tangent function such as

$$\tan^{-1}(x) \approx x - \frac{1}{3}x^3 + \dots$$

- Angle can be approximated as

$$\theta(t) \approx 2\pi f_c t + \beta \sin(2\pi f_m t) - \frac{1}{3}\beta^3 \sin^3(2\pi f_m t)$$

- Ideally, we should have

$$\theta(t) \approx 2\pi f_c t + \beta \sin(2\pi f_m t)$$

- The harmonic distortion value is

$$D(t) = \frac{\beta^3}{3} \sin^3(2\pi f_m t)$$

- The maximum absolute value of D(t) is

$$D_{\max} = \frac{\beta^3}{3}$$

- For example for  $\beta = 0.3$ ,

$$D_{\max} = \frac{0.3^3}{3} = 0.009 \approx 1\%$$

which is small enough for it to be ignored in practice.

# Amplitude Distortion of Narrow-band FM

- Ideally, FM wave has a constant envelope
  - But, the modulated wave produced by the narrow-band FM differ from this ideal condition in two fundamental respects:
    - The envelope contains a residual amplitude modulation that varies with time
    - The angle  $\theta_i(t)$  contains harmonic distortion in the form of third- and higher order harmonics of the modulation frequency  $f_m$

# Wide-Band Frequency Modulation

- Spectral analysis of the wide-band FM wave

$$s(t) = A_c \cos[2\pi f_c t + \beta \sin(2\pi f_m t)]$$

or

$$s(t) = \Re [A_c \exp[j2\pi f_c t + j\beta \sin(2\pi f_m t)]] = \Re[\tilde{s}(t) \exp(j2\pi f_c t)]$$

where  $\tilde{s}(t) = A_c \exp [j\beta \sin(2\pi f_m t)]$  is called “complex envelope”.

Note that the complex envelope is a periodic function of time with a fundamental frequency  $f_m$  which means

$$\tilde{s}(t) = \tilde{s}(t + kT_m) = \tilde{s}(t + \frac{k}{f_m})$$

where  $T_m = 1/f_m$

- Then we can rewrite

$$\begin{aligned}\tilde{s}(t) &= \tilde{s}(t + k/f_m) \\ &= A_c \exp[j\beta \sin(2\pi f_m(t + k/f_m))] \\ &= A_c \exp[j\beta \sin(2\pi f_m t + 2k\pi)] \\ &= A_c \exp[j\beta \sin(2\pi f_m t)]\end{aligned}$$

- Fourier series form

$$\tilde{s}(t) = \sum_{n=-\infty}^{\infty} c_n \exp(j2\pi n f_m t)$$

where

$$\begin{aligned}c_n &= f_m \int_{-1/(2f_m)}^{1/(2f_m)} \tilde{s}(t) \exp(-j2\pi n f_m t) dt \\ &= f_m A_c \int_{-1/(2f_m)}^{1/(2f_m)} \exp[j\beta \sin(2\pi f_m t) - j2\pi n f_m t] dt\end{aligned}$$



- Define the new variable:  $x = 2\pi f_m t$

Then we can rewrite

$$c_n = \frac{A_c}{2\pi} \int_{-\pi}^{\pi} \exp[j(\beta \sin x - nx)] dx$$

- $n$ th order Bessel function of the first kind and argument  $\beta$

$$J_n(\beta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \exp[j(\beta \sin x - nx)] dx$$

- Accordingly

$$c_n = A_c J_n(\beta)$$

which gives

$$\tilde{s}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \exp(j2\pi n f_m t)$$

- Then the FM wave can be written as

$$\begin{aligned}
 s(t) &= \Re[\tilde{s}(t) \exp(j2\pi f_c t)] \\
 &= \Re \left[ A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \exp[j2\pi n(f_c + f_m)t] \right] \\
 &= A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos[2\pi(f_c + n f_m)t]
 \end{aligned}$$

- Fourier transform

$$S(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [\delta(f - f_c - n f_m) + \delta(f + f_c + n f_m)]$$

which shows that the spectrum consists of an infinite number of delta functions spaced at  $f = f_c \pm n f_m$  for  $n = 0, +1, +2, \dots$

# Properties of Single-Tone FM for Arbitrary Modulation Index $\beta$

1. For different values of  $n$

$$J_n(\beta) = J_{-n}(\beta), \quad \text{for } n \text{ even}$$

$$J_n(\beta) = -J_{-n}(\beta), \quad \text{for } n \text{ odd}$$

2. For small value of  $\beta$

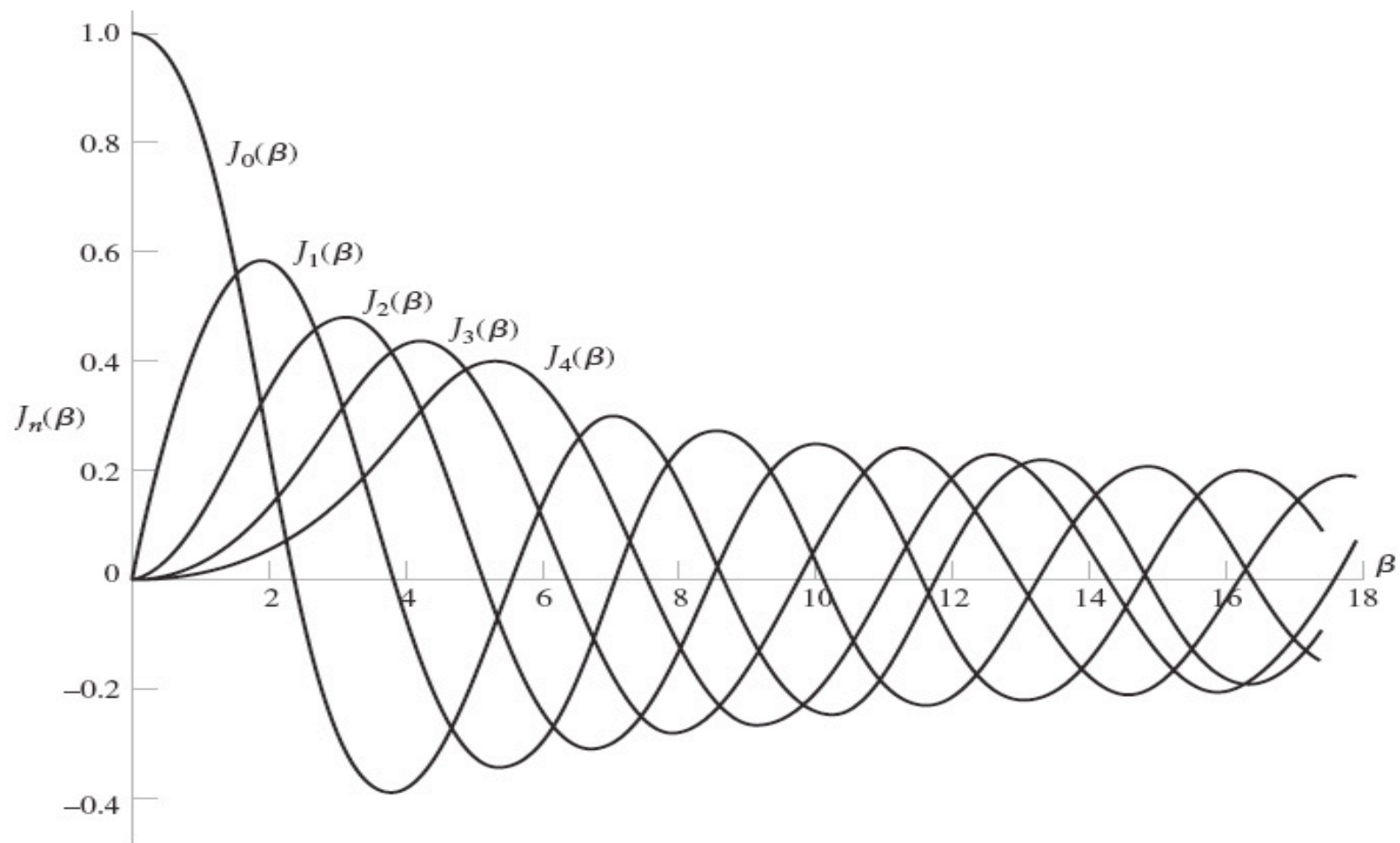
$$J_0(\beta) \approx 1,$$

$$J_1(\beta) \approx \frac{\beta}{2}$$

$$J_n(\beta) \approx 0, \quad n > 2$$

6. The equality holds exactly for arbitrary  $\beta$

$$\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$$



**FIGURE 4.6** Plots of the Bessel function of the first kind,  $J_n(\beta)$ , for varying order  $n$ .

[Ref: Haykin & Moher, Textbook]

1. The spectrum of an FM wave contains a carrier component and an infinite set of side frequencies located symmetrically on either side of the carrier at frequency separations of  $f_m, 2f_m, 3f_m \dots$
2. The FM wave is effectively composed of a carrier and a single pair of side-frequencies at  $f_c \pm f_m$  .
3. The amplitude of the carrier component of an FM wave is dependent on the modulation index  $\beta$  . The average power of such a signal developed across a 1-ohm resistor is also constant:

$$P_{av} = \frac{1}{2} A_c^2$$

The average power of an FM wave may also be determined from

$$P_{av} = \frac{1}{2} A_c^2 \sum_{n=-\infty}^{\infty} J_n^2(\beta)$$